

Selective higher order fiber mode excitation using a monolithic setup of a phase plate at a fiber facet

Photonics West 2015
Laserresonators, Microresonators and Beamcontrol XVII
9343-56

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We selectively excited different higher order fiber modes using different setups of a passive binary phase plate in front of the input facet of an optical fiber. The achieved results were analyzed by a complete modal decomposition of the field emitted by the fiber.

Motivation

- higher order fiber modes in an optical fiber show a quite strong dependence on external disturbances^[1,2]
- for a possible utilization in an uncomplex sensor the excitation of pure higher order modes [HOMs] will be necessary
- passive binary phase^[3] plates promise a reproducibly manufacturable, robust, efficient^[4,5] and rather cheap setup
- in order to avoid the free space propagation losses in the usually employed free space setups^[4-6] we put the phase plate directly in front of the fiber input facet [“monolithic setup”]

Fiber Modes

- fiber modes are constant field distributions all along the fiber [eigenfunctions]
- all guided fields are describable as a superposition of the modes [orthonormal basis]
- for a weakly guiding fiber and in the paraxial case a fiber guides the so called *LP*-modes

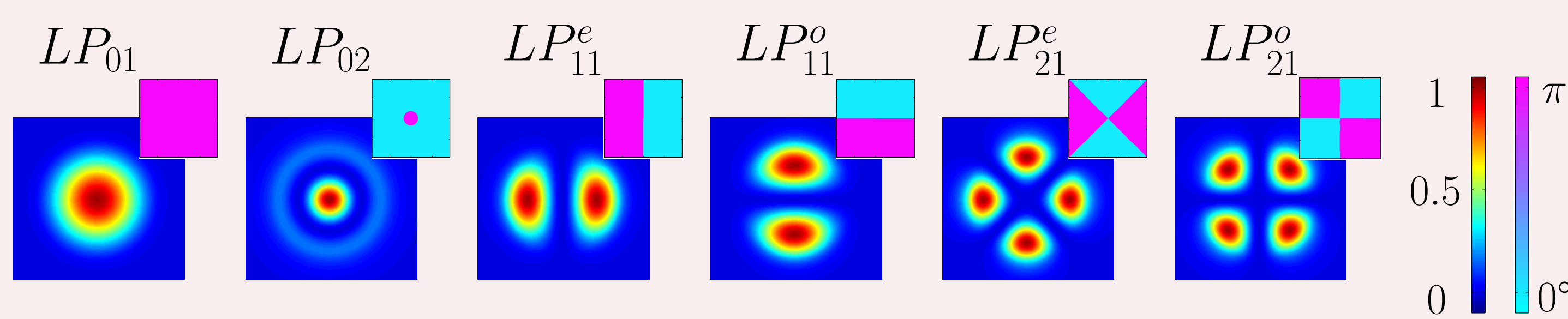


Figure 1: Intensity and phase [insets] profiles of the guided *LP*-modes calculated numerically.

Passive Binary Phase Plates

- incoming fundamental Gaussian beam with its waist at the position of the phase plate
- laterally varying thickness induces laterally varying phase shift

$$\Delta\Phi = [n_{ph} - n] \frac{d}{\lambda_0} 2\pi$$

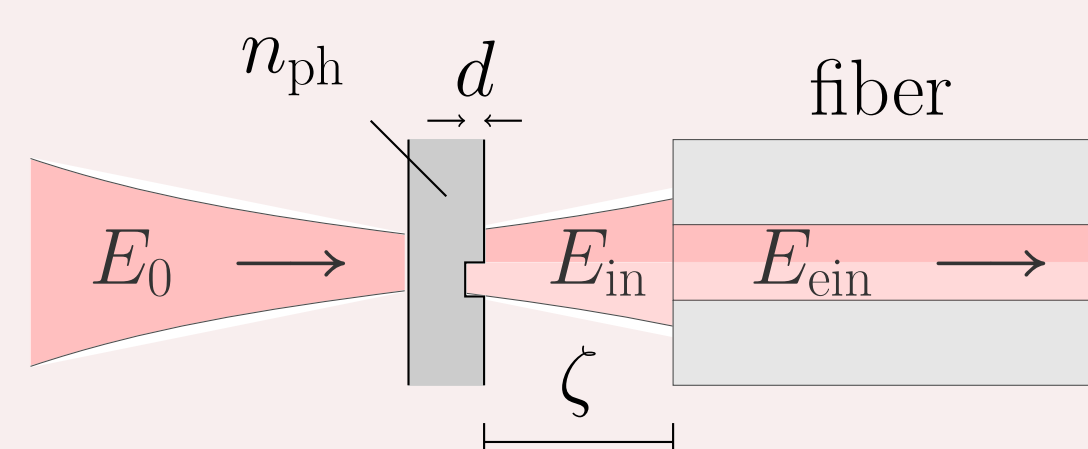


Figure 2: Principle setup of the monolithic binary phase plate in front of the fiber input facet.

- investigated transversal phase profiles

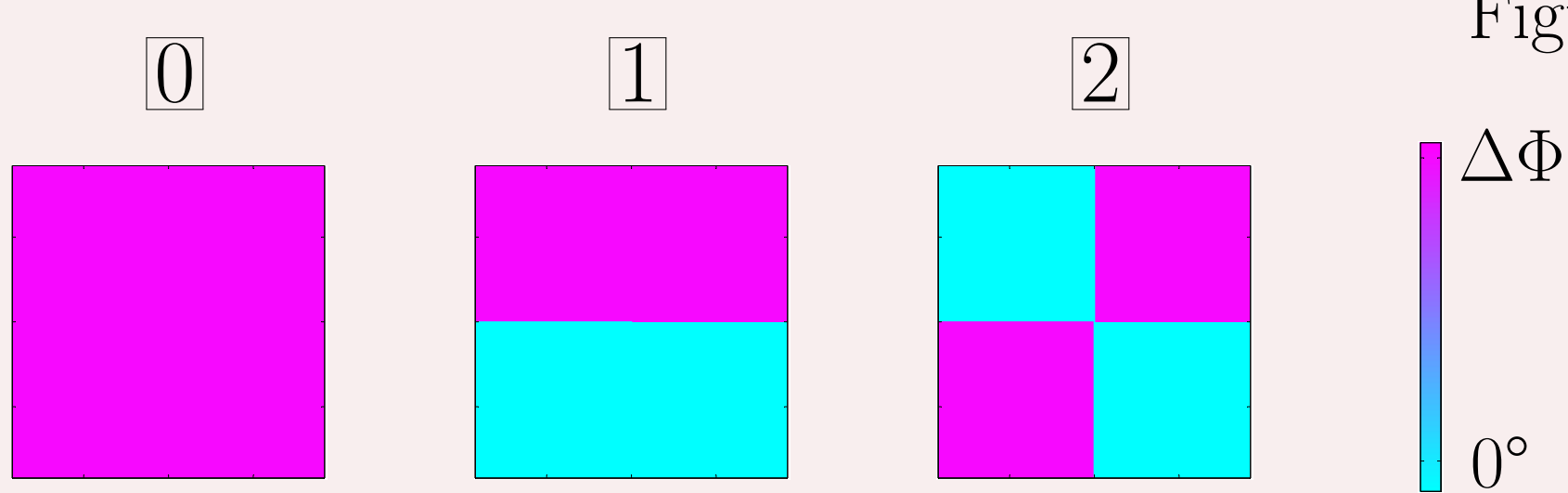


Figure 3: Transversal profiles of the used phase plates.

- one should note that the upper limit of the $\Delta\Phi$ -scale in figure 3 is due to experimental difficulties not mandatorily 180°
- the power percentage of the field E_{in} [see figure 2], after a phase plate [1] with phase shift $\Delta\Phi$, adapted to the mode group LP_{lm} corresponds to

$$\tilde{\rho}_l^2 = \frac{1}{2} [1 - \cos(\Delta\Phi)] \quad , \quad \tilde{\rho}_0^2 = \frac{1}{2} [1 + \cos(\Delta\Phi)]$$

Experimental Setup

- the decomposition of the fields excited in the fiber was achieved by analyzing the output beam via the correlation filter method [CFM]^[7]

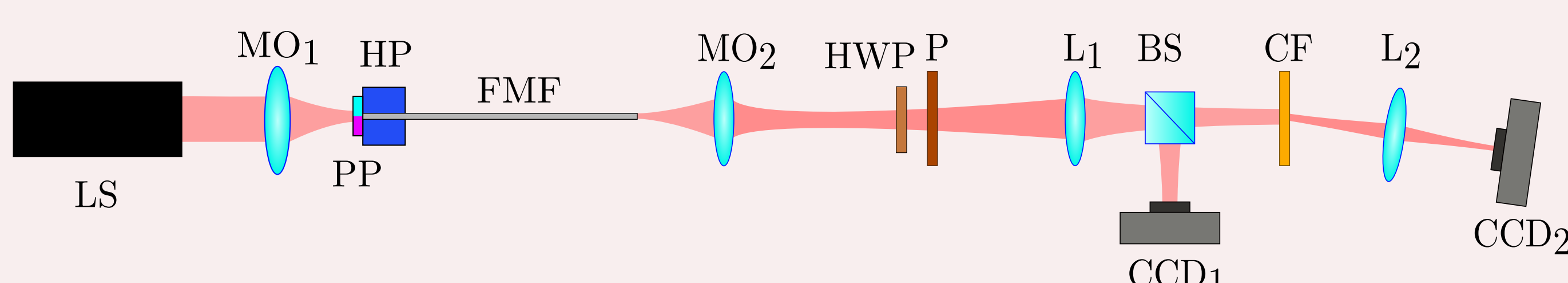


Figure 4: Scheme of the experimental setup [LS - laser source, $MO_{1,2}$ - microscope objectives, PP - phase plate, HP - Hexapod, FMF - few mode fiber, HWP - $\frac{\lambda}{2}$ waveplate, P - polarizer, $L_{1,2}$ - lenses, BS - beam splitter, $CCD_{1,2}$ - cameras, CF - correlation filter].

Results

- for the investigated phase plates the remaining free space propagation distance ζ [see figure 2] between the phase plate and the fiber input facet of less than $100 \mu\text{m}$ showed to be negligible
- the numerical experiments show a high efficiency and an achievable mode purity of 100%

Table 1: Numerically determined parameters of the monolithic setups assuming $\Delta\Phi = 180^\circ$

phase plate	efficiency	σ_{max}	FWHM
[0]	99.3%	$10.0 \mu\text{m}$	$16.6 \mu\text{m}$
[1]	72.9%	$12.7 \mu\text{m}$	$18.2 \mu\text{m}$
[2]	67.2%	$15.1 \mu\text{m}$	$24.6 \mu\text{m}$

- dependence of the modal content on the transversal displacement of the incident beam, exemplarily seen in figure 5 for phase plate [1], shows a good agreement

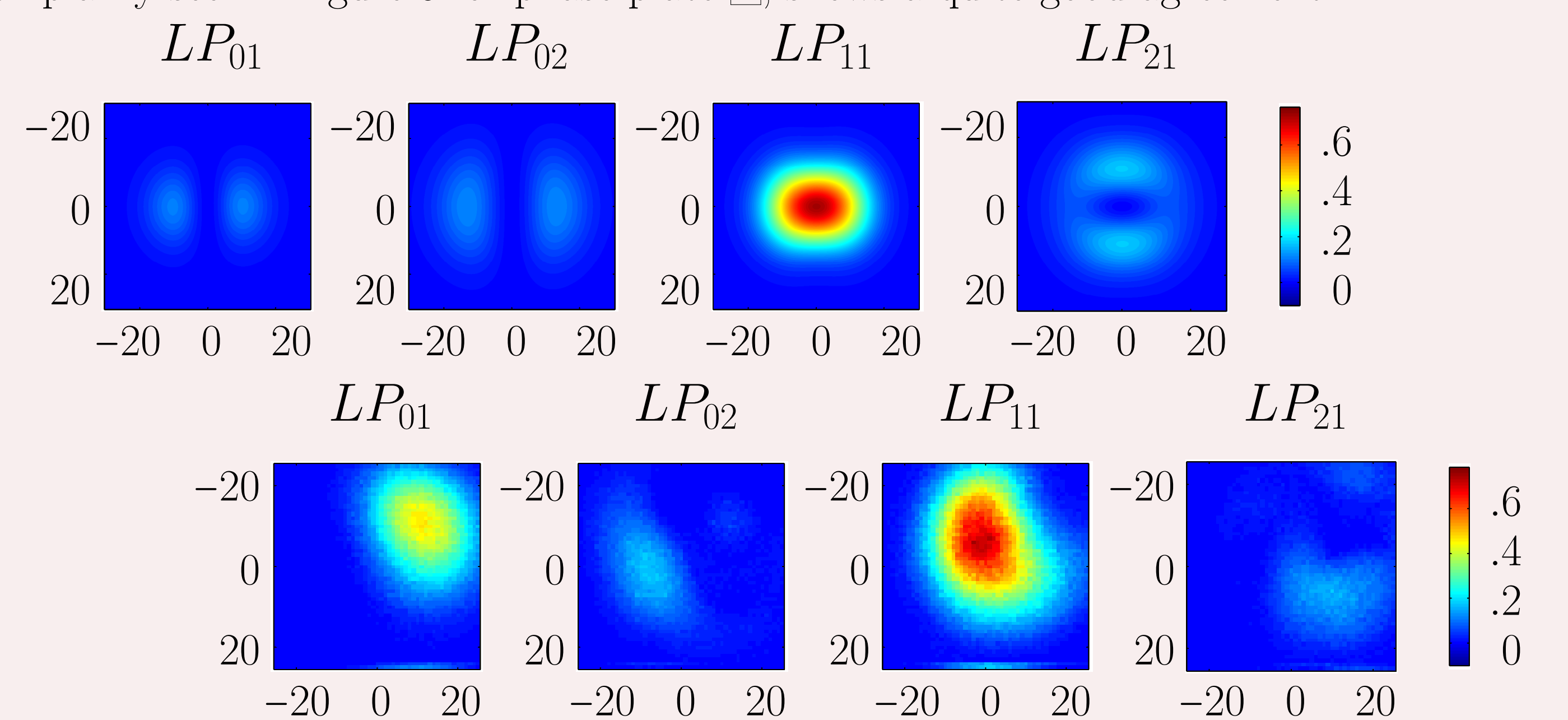


Figure 5: Modal coupling efficiency for the numerical [$\Delta\Phi = 180^\circ$, top] and the optical [bottom] experiments as function of the transversal displacement of the incoming beam relative to the concentric position of incident beam and fiber for phase plate [1].

Comparison

- the non-monolithic setup showed to be slightly more frail to misalignments or disturbances
- the optimal coupling efficiencies show the monolithic setup to be more efficient [approximately by a factor of 2, $\Delta\Phi_{\text{free space}} = 180^\circ$, $\Delta\Phi_{\text{monolithic}} \lesssim 150^\circ$]

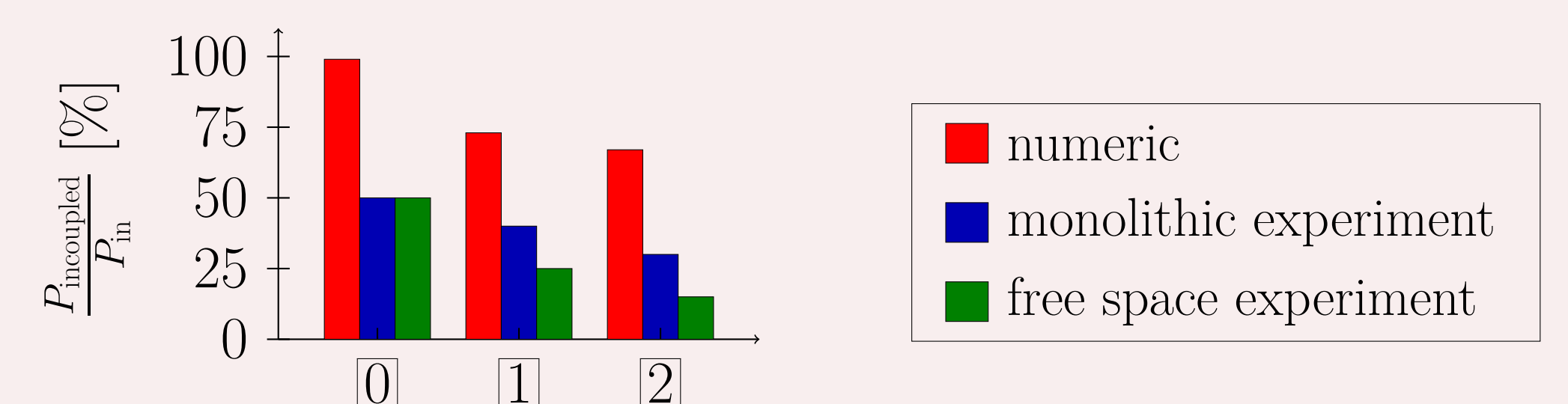


Figure 6: Numerical and experimental optimal coupling efficiencies.

Conclusion

- a proof of principle for the monolithic setup is given
- although the phase shift of the phase plate was not optimal, the monolithic setup was already more efficient
- outlook:
 - optimization of the phase shift $\Delta\Phi$
 - investigation of the influence of a possible tilt of the incident beam
 - determination of external effects [e.g. pressure, strain or temperature] on the different fiber modes in order to be able to use it as a sensor

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